# GLAST <br> Guidance, Navigation \& Control System 

Jennifer M. Bracken<br>Code 571/GN\&C System Engineering Branch

## Assumptions

- Attitude:
- Orbit Period:
- Inclination:

550 Km
5739 sec
28.5 deg

From IMDC Session in August 1998:

- Inertias:

2742, 3341, 3363 Kg-m ${ }^{2}$

- CPCG Offset:
- Solar Array Area:
.33 m
$17.4 \mathrm{~m}^{2}$


## GN\&C Component Selection Drivers

- Star Trackers (attitude knowledge)
- Gyros (attitude knowledge)
- Coarse Sun Sensors
- Reaction Wheels (slew requirements)
- Torquer Bars (disturbance torques)
- Magnetometers
- GPS Receiver/Antennas (orbit knowledge)


## Component Trades

- Star Trackers
- 5 arcsec knowledge requirement in all 3 axes
- 2 are necessary to meet requirement
- 3 arcsec accuracy along off-boresight axes
- 30 arcsec accuracy along boresight
- 3 for redundancy
- Gyros
- 5 arcsec knowledge requirement during slews
- Low noise and minimal drift

Predicted Kalman Filter Update Performance using Farrenkopf's Equations from AIAA Journal Guidance \& Control (July 78)
(Note: This is based on SIRU and CT-602 noise specifications only. It does not take into account misalignments)

| Kalman Filter Update Time (sec) | 0.2 | 0.5 | 1 | 0.2 | 0.5 | 1 | 0.2 | 0.5 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Std Dev Attitude Angle (arcsec) | 0.87377 | 0.89116 | 0.91966 | 0.87377 | 0.89116 | 0.91966 | 0.87377 | 0.89116 | 0.91966 |
| Std Dev Drift Rate Bias (arcsec/sec) | 0.00131 | 0.00132 | 0.00134 | 0.00131 | 0.00132 | 0.00134 | 0.00131 | 0.00132 | 0.00134 |
|  | 6 min Slew |  |  | 12 min Slew |  |  | Sun in FOV |  |  |
| Time Duration of No Updates (sec) | 360 | 360 | 360 | 720 | 720 | 720 | 956.5 | 956.5 | 956.5 |
| Angle Buildup during No Update Period (arcsec) | 1.09799 | 1.10008 | 1.10237 | 1.71446 | 1.71981 | 1.72569 | 2.10181 | 2.10951 | 2.11796 |

## Component Trades (cont.)

- Reaction Wheels
- Must be able to satisfy slewing requirements
- 90 deg in 6 min: 16 N-m, 14.7 (29.4) N-m-s
- 70 deg in 5 min: . $18 \mathrm{~N}-\mathrm{m}, 13.7$ (27.4) N-m-s


- Must be able to accommodate external disturbances
- Gravity Gradient:
- Aerodynamic:
- Solar:
- Disturbance Totals:
. $0022 \mathrm{~N}-\mathrm{m}, 12.7 \mathrm{~N}-\mathrm{m}-\mathrm{s} /$ orbit
. $00027 \mathrm{~N}-\mathrm{m}, 1.5 \mathrm{~N}-\mathrm{m}-\mathrm{s} /$ orbit
$.000078 \mathrm{~N}-\mathrm{m}, .045 \mathrm{~N}-\mathrm{m}-\mathrm{s} /$ orbit
. $0026 \mathrm{~N}-\mathrm{m}, 14.7 \mathrm{~N}-\mathrm{m}-\mathrm{s} /$ orbit


## Component Trades (cont.)

- Torquer Bars
- Must be able to accommodate external disturbances
- Required dipole: $107 \mathrm{Am}^{2}$, double (even triple) to account for uncertainties
- If inertias and cpcg offset change by $\mathbf{1 0 \%}$ for the worse, the external disturbances will increase by about 7 N -m-s/orbit, and the dipole required to unload momentum will increase by about $50 \mathrm{Am}^{2}$
- Torquer Bar Size and Momentum Unloading:
- $100 \mathrm{Am}^{2}$ bars will be able to unload 13.7 N -m-s per orbit.
- $230 \mathrm{Am}^{2}$ bars will be able to unload 31.6 N -m-s per orbit.
- $300 \mathrm{Am}^{2}$ bars will be able to unload 41.2 N -m-s per orbit.


## GN\&C Mass, Power \& Cost Estimates

| Components | Qty | Make/Model | Mass per Unit (Kg) | Avg Power per Unit <br> (W) | Peak Power per Unit <br> (W) | Cost per Unit (\$K) | Total Mass <br> (Kg) | Total <br> Avg <br> Power <br> (W) | Total <br> Peak <br> Power <br> (W) | Total <br> Cost <br> (\$K) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Star Tracker | 3 | Ball CT-602 | 5.41 | 8.0 | 9.0 | 650 | 16.23 | 24.0 | 27.0 | 1950 |
| Inertial Reference Unit (4 Axis) | 1 | Litton SIRU (HRG) | 5.45 | 22.0 | 22.0 | 1200 | 5.45 | 22.0 | 22.0 | 1200 |
| Coarse Sun Sensors | 8 | Adcole 11866 | 0.0046 | 0.0 | 0.0 | 6 | 0.0368 | 0.0 | 0.0 | 48 |
| Reaction Wheels | 4 | Ithaco Type E | 13.90 | 40.0 | 280.0 | 350 | 55.60 | 160.0 | 1120.0 | 1400 |
| Torquer Bars (Dual Wound) | 3 | Ithaco TR230CFR | 5.20 | 3.8 | 5.4 | 38 | 15.60 | 11.4 | 16.2 | 113 |
| Magnatometers | 2 | Ithaco IM-203 | 0.704 | 1.4 | 1.7 | 61 | 1.408 | 2.8 | 3.4 | 122 |
| GPS Receiver/Antenna Bundle | 2 | Motorola Viceroy | 1.83 | 4.8 | 4.8 | 120 | 3.66 | 9.6 | 9.6 | 240 |
| ACE (2 Units in 1 Housing) | 1 | TRMM (In-house) | 25.00 | 7.5 | 12.5 | 2700 | 25.00 | 7.5 | 12.5 | 2700 |
|  |  |  |  |  | Grand Totals = |  | 123.0 | 237.3 | 1210.7 | 7773 |

## GN\&C Mode Requirements

- Initial Acquisition
- Null rates and acquire sun on solar arrays
- Mission Modes
- Maintain roll-canted zenith attitude with varying yaw angle (to accommodate thermal and power) for first year of mission (90 deg slews in 6 min )
- Maneuver and maintain inertial attitudes on selected targets for the remaining years of the mission ( $\mathbf{7 0} \mathbf{~ d e g}$ slews in 5 min )
- Accommodate observation of Gamma Ray Bursts when necessary (70 deg slews in 5 min)
- Safe Hold
- Provide power and thermally safe independent "safety net" in case of anomalies


## E-Wheel Power Profile during Sky Survey



## E-Wheel Power Profile during Sky Survey



## E-Wheel Power Profile during Sky Survey



## Potential Jitter Sources

- Reaction wheel imbalances
- Imbalance specifications for the Ithaco E wheel results in spacecraft jitter at sub-arcsec level
- Wheel isolation packages are available if necessary
- Reaction wheel zero speed crossings
- With 4 wheels, zero speed crossings are minimized
- Will be able to account for this from post processed data
- Solar array induced jitter
- Expect no problem - but will require verification by detailed analysis when spacecraft and instrument structural models are available
- Gimbaled antenna induced jitter
- Expect no problem - but will require verification by detailed analysis when spacecraft and instrument structural models are available

